



# **Candlestick (Open) Flare Emission Test Summary Report**

*Prepared for:*

**Cornerstone Environmental**

Evergreen Recycle and Disposal Facility  
2625 East Broadway  
Northwood, Ohio 43619

Project No. 07-3600.00  
July 9, 2007

BT Environmental Consulting, Inc.  
2615 Wolcott Street  
Ferndale, Michigan 48220  
(248) 548-8070



### Executive Summary

BT Environmental Consulting, Inc. (BTEC) was retained by Cornerstone Environmental Group, LLC (Cornerstone) to conduct a compliance test program for one candlestick (open) flare at a landfill located in Northwood, Ohio. The purpose of the test program was to provide data too Cornerstone for use in demonstrating compliance with the requirements outlined in Title 40, Part 60, Subpart WWW of the Code of Federal Regulations (40 CFR 60, Subpart WWW).

The fieldwork, conducted May 31, 2007, was performed in accordance with BTEC's proposal, 071852B, dated April 17, 2007. Mr. Mark Westerberg, Senior Project Manager; and Mr. Brandon Chase, Environmental Engineer, conducted the testing. Mr. Matt Boudreau, with Cornerstone, provided the on-site coordination for the testing. Ms. Wendy Licht, with the Ohio Environmental Protection Agency, was onsite to observe the testing. The results of the emissions testing are highlighted below:

Parameter	Applicable Requirement	Average Result
Flare Exhaust Gas Exit Velocity (feet/second)	<b>&lt;60</b>	<b>31.6</b>
Flare Exhaust Smoke Emissions (Visual Emissions in a 2-hour period)	<b>None</b>	<b>None</b>
Flare Inlet Gas Heating Value (MJ/scm)	<b>&gt;7.45</b>	<b>17.55</b>

MJ: megajoules  
scm: standard cubic meters



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## **1.0 Introduction**

BT Environmental Consulting, Inc. (BTEC) was retained by Cornerstone Environmental Group, LLC (Cornerstone) to conduct a compliance test program for one candlestick (open) flare at the Evergreen Recycling & Disposal facility (RDF) landfill located in Northwood, Ohio. The purpose of the test program was to provide data to Cornerstone for use in demonstrating compliance with the requirements outlined in Title 40, Part 60, Subpart WWW of the Code of Federal Regulations (40 CFR 60, Subpart WWW).

Field sampling for the emissions test program was conducted on May 31, 2007. Mr. Mark Westerberg, Senior Project Manager; and Mr. Brandon Chase, Environmental Engineer, conducted the testing. Mr. Matt Boudreau, with Cornerstone, provided the on-site coordination for the testing. Ms. Wendy Licht, with the Ohio Environmental Protection Agency, was onsite to observe the testing.

## **2.0 Process Description**

The Evergreen Recycling & Disposal Facility (RDF) employs a candlestick (open) flare to burn landfill gas extracted by a network of extraction wells (see Figure 1 for a schematic of the flare). The flare is rated at 4,300 scfm.

## **3.0 Sampling and Analytical Methodologies**

Sampling and analytical methodologies for the emissions test program can be separated into two categories as follows:

- (1) Measurement of exhaust gas velocity, and molecular weight;
- (2) Measurement of Fugitive Emissions

Descriptions of sampling and analytical methodologies by category are summarized by Sections 3.1 and 3.2, respectively.

### **3.1 Exhaust Gas Velocity, Molecular Weight, and Moisture Content**

Measurement of exhaust gas velocity, molecular weight, and moisture content was conducted using the following reference test methods codified at Title 40, Part 60, Appendix A of the Code of Federal Regulations (40 CFR 60, Appendix A):

- Method 1 - *"Location of the Sampling Site and Sampling Points"*
- Method 2 - *"Determination of Stack Gas Velocity and Volumetric Flowrate"*
- Method 3C - *"Determination of carbon dioxide, methane, nitrogen, and oxygen from stationary sources"*

Note: Stack gas velocities were provided by the facility utilizing the facilities flow continuous emissions monitoring system (cems). Production data including flare inlet flowrate, and landfill gas feed rate are provided in Appendix A. Stack gas velocity traverses could not be conducted



by BTEC in accordance with the procedures outlined in Method 1 and Method 2 due to the absence of a sampling port 90-degrees from the sampling port on the horizontal axis of the duct. However, as a check of the facilities flow cems a traverse was conducted on the horizontal sampling port utilizing a standard pitot tube and thermocouple assembly, calibrated in accordance with Method 2, Section 4.1.1, to measure exhaust gas velocity pressures (using an incline manometer and pyrometer) during testing (see Appendix C for results). The standard pitot tube dimensions were within specified limits, therefore, a baseline pitot tube coefficient of 0.99 (dimensionless) was assigned.

The flare inlet gas molecular weight and heating value was evaluated using USEPA Method 3C, "Determination of Carbon Dioxide, Methane, Nitrogen, and Oxygen from Stationary Sources". Three 30-minute integrated samples were extracted from the flare inlet gas stream using a stainless steel probe and an evacuated cylinder (see Figure 2 for a schematic of the sampling train). Triangle Environmental Services (TES) analyzed the samples utilizing a gas chromatograph equipped with a thermal conductivity detector. Molecular weight was calculated using the method outlined in Section 12.0 of USEPA Method 3. Heating value was calculated according to the method detailed in Title 40 of the Code of Federal Regulations, Part 60.18. The laboratory analytical data pertaining to the USEPA Method 3C analysis are available in Appendix B. Moisture content of the gas stream was determined by USEPA Method 3C analysis. The field data sheets relating to these analyses can be viewed in Appendix C.

### **3.2 Flare Exhaust Smoke Emissions (USEPA Method 22)**

Visual Emissions from the operation of the flare were evaluated according to USEPA Method 22, "Visual Determination of Fugitive Emissions from Material Sources and Smoke Emissions from Flares". The frequency and length of time that visible emissions were observed was recorded during the course of one 2-hour observation period. Field data relating to this test method are available in Appendix D.

## **4.0 Test Results**

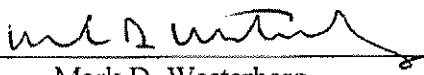
The performance requirements of 40 CFR 60.18 with respect to an open non-assisted flare for which compliance must be demonstrated by this testing are (1) the exhaust gas exit velocity must be less than 60 feet per second (fps), and (2) the net heating value of the gas stream being combusted in the flare must be greater than 7.45 megajoules per standard cubic meter (MJ/scm). The average values of exit velocity and net heating value indicated by this testing were 31.6 fps, and 17.55 MJ/scm, respectively. The tested flare exhaust stack is therefore in compliance with 40 CFR 60.18. Raw field and computer-calculated data used in the determination of the flare exit velocity, laboratory analytical utilized to calculate net heating values, as well as all equipment calibration, and flare operational data are available in the appendices. Sample calculations are presented in Appendix E.



### **Limitations**

The information and opinions rendered in this report are exclusively for use by Cornerstone. BTEC will not distribute or publish this report without Cornerstone's consent except as required by law or court order. BTEC accepts responsibility for the competent performance of its duties in executing the assignment and preparing reports in accordance with the normal standards of the profession, but disclaims any responsibility for consequential damages.

This report was prepared by:   
Brandon Chase  
Staff Environmental Engineer

This report was reviewed by:   
Mark D. Westerberg  
Senior Project Manager



**Table 1**  
**Flare Inlet Gas Stream Volumetric Flowrate and Exit Velocity**  
**Evergreen Recycling and Disposal Facility**  
**Northwood, OH**  
**BTEC Project No. 07-3600.00**  
**May 31, 2007**

Parameter	Test 1	Test 2	Test 3	Average
Sample Time	10:16	10:48	11:20	
Flare Inlet Gas Volumetric Flowrate (scfm)	2,009	1,983	2,093	2,028
Flare Tip Diameter (in.)	14.0	14.0	14.0	
Flare Tip Cross-Sectional Area (ft <sup>2</sup> )	1.07	1.07	1.07	
Allowable V <sub>max</sub> (fps) <sup>1</sup>	60	60	60	60
Flare Gas Exit Velocity (fps)	31.3	30.9	32.6	31.6

<sup>1</sup> from 40 CFR 60.18(c)(4)(i)  
scfm : standard cubic feet per minute  
in. : inches  
fps : feet per second



**Table 2**  
**Flare Inlet Gas Net Heating Value**  
**Evergreen Recycling and Disposal Facility**  
**Northwood, Ohio**  
**BTEC Project No. 07-3600.00**  
**May 31, 2007**

Parameter	Test 1	Test 2	Test 3	Average
Flare Inlet Gas Methane Content (ppm)	558,380	555,759	468,223	527,454
Flare Inlet Gas Methane Content (%)	55.8	55.6	46.8	52.7
Methane Molecular Weight (lb/lb mol)	16	16	16	
Methane Heating Value (kcal/g) <sup>1</sup>	11.9533	11.9533	11.9533	
Methane Heating Value (kcal/g mol)	191.3	191.3	191.3	
Flare Inlet Gas Minimum Net Heating Value Requirement (MJ/scm) <sup>2</sup>	7.45	7.45	7.45	7.45
Flare Inlet Gas Net Heating Value (MJ/scm)	18.58	18.49	15.58	17.55

<sup>1</sup> USEPA Office of Air Quality Planning and Standards' Control Cost Manual

<sup>2</sup> from 40 CFR 60.18(c)(3)(ii)

ppm : parts per million volume

kcal/g : kilocalories per gram

kcal/g mol : kilocalories per gram mole

MJ/scm : megajoules per standard cubic meter






# USEPA Method 3C

Stack or Duct Being Tested

Flow Controller

Evacuated Summa  
Canister

 <b>BTEC Inc.</b>		<b>B.T. Environmental Consulting Inc.</b>	
Project No. 07-3600.00		2615 Wolcott Street Ferndale, Michigan 48220 (248) 548 - 8070	
Client Cornerstone Evergreen Northwood, OH		Source Flare	
Date 6-29-07	Scale Not to Scale	Figure No. 2	



DAQSTANDARD R6.03  
 Data Viewer R6.03  
 WASTE MANAGEMENT INC WMI-User

115-00009-\*\*\*\*

Device Type FX100  
 Serial No. S5DA05308  
 File Message  
 Time Correction None  
 Starting Condition Auto  
 Dividing Condition Auto  
 Meas Ch. 3  
 Math Ch. 2  
 Data Count 96  
 Sampling Interval 600.000 sec  
 Start Time 2007/05/31 11:00:00 0.000  
 Stop Time 2007/06/01 02:50:00 0.000  
 Trigger Time 2007/05/31 14:50:00 0.000  
 Trigger No. 23  
 Damage Check Not Damaged

Converted Group 1 - 1

Date	Time	Ch. Tag sec	CH01 FLARE TEMP F	CH02 FLOW SCFM	CH03 VACUUM INCHES	CH31 TOTAL FLOW *100 SCF
2007/05/31	09:50:00	0.000	1425	472	-8.0	4178484
2007/05/31	10:00:00	0.000	1425	2021	-28.5	4178670
2007/05/31	10:10:00	0.000	1424	1999	-29.3	4178872
2007/05/31	10:20:00	0.000	1426	1994	-29.1	4179071
2007/05/31	10:30:00	0.000	1455	2002	-28.8	4179271
2007/05/31	10:40:00	0.000	1455	2028	-28.4	4179469
2007/05/31	10:50:00	0.000	1424	1973	-29.1	4179668
2007/05/31	11:00:00	0.000	1424	1977	-28.8	4179866
2007/05/31	11:10:00	0.000	1451	1963	-29.0	4180063
2007/05/31	11:20:00	0.000	1422	1964	-28.4	4180256
2007/05/31	11:30:00	0.000	1425	1987	-29.5	4180467
2007/05/31	11:40:00	0.000	1479	2191	-28.8	4180687
2007/05/31	11:50:00	0.000	1467	2202	-27.6	4180909
2007/05/31	12:00:00	0.000	1435	1991	-28.6	4181113
2007/05/31	12:10:00	0.000	1470	1988	-28.6	4181311
2007/05/31	12:20:00	0.000	1466	1946	-27.6	4181506
2007/05/31	12:30:00	0.000	1431	1906	-28.1	4181701
2007/05/31	12:40:00	0.000	1441	1959	-28.0	4181896
2007/05/31	12:50:00	0.000	1456	1934	-27.2	4182089

Test	Time	Ave Flow scfm
Run-1	10:00-10:40	2009
Run-2	10:40-11:30	1982
Run-3	11:30-12:00	2093



## Method 3-C Analytical Results

prepared for

### BT ENVIRONMENTAL

2615 Wolcott  
Ferndale, MI 48220

by

### Triangle Environmental Services, Inc.

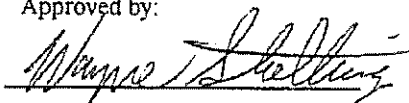
We, the undersigned, certify to the best of our knowledge that all analytical data presented in this report have been checked for completeness; that the results are accurate, error-free, legible, and have been obtained in accordance with approved protocol; and that all deviations and analytical problems are summarized in the "Comments on the Analyses" page(s).

Reviewed by:



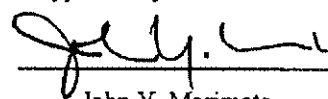
Donna Nolen-Weathington  
Method 25 Supervisor

Approved by:



Wayne A. Stollings  
President

Approved by:



John Y. Morimoto  
QA Officer

Report  
**07140-25C**

June 12, 2007



**Triangle Environmental Services, Inc.**  
**COMMENTS ON THE ANALYSES**

Report #07140-25C for BT Environmental  
Project ID: Cornerstone 07-3600.00

---

Tanks Received: 6/1/07

Samples Analyzed: 6/4/07  
Client Chain-of-Custody forms: 1 p

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All samples: Laboratory preshipment and receipt pressure and temperature readings were used for the tank pre- and post-test tank data, respectively. Also, laboratory receipt barometric pressure and temperature data were used to determine the water vapor fraction.

# TRIANGLE ENVIRONMENTAL SERVICES, INC. METHOD 3-C TABLE OF RESULTS

Name: BT Environmental

ID#07140-25C

Analyzed: 6/4/07

Project ID: Cornerstone 07-3600.00

Sample Description	Concentrations (ppm)			
	O2	N2	CH4	CO2
1 Flare Inlet Run 1	11482	57009	558380	381077
2 Flare Inlet Run 2	11704	57907	555759	379565
3 Flare Inlet Run 3	43712	171329	468223	320690

# **Triangle Environmental Services, Inc.**

## **METHOD 3-C PROCEDURES**

Report #07140-25C

### **CALIBRATION**

Triplicate injections of a calibration gas mixture consisting of oxygen ( $\approx 2.5\%$ ), nitrogen ( $\approx 10\%$ ), carbon dioxide ( $\approx 25\%$ ), and methane ( $\approx 2\%$ ) are made immediately before and after each batch of samples. Daily response factors are calculated from the pre-batch integrated responses (average area count / concentration in ppm) and must agree within 20% of the response factors of the initial calibrations. Further, the post-batch response factors must agree within 5% of the pre-batch response factors. Both criteria must be met before the analyses are considered valid.

### **ANALYSIS**

All samples, which include the daily calibration gas mixture and sample tanks, are analyzed in triplicate using a computer-interfaced gas chromatograph equipped with an automated gas sampling system and a thermal conductivity detector (TCD).  $O_2$ ,  $N_2$ ,  $CO$ ,  $CH_4$ , and  $CO_2$  are eluted from the column and pass to the TCD.

### **CALCULATIONS**

Calculations are done in accord with USEPA Method 3-C procedures. A sample calculation for one of the samples is provided in the report.

### **EQUIPMENT**

Tanks are at a minimum twice evacuated and filled with ambient air filtered through charcoal and are then evacuated to below 10 mm Hg and monitored for at least an hour to check that the tanks do not leak more than 1 mm Hg/hour. They are then pressurized to greater than ambient pressure with helium, analyzed to ensure  $< 2$  ppm  $CH_4$  and  $< 20$  ppm  $CO_2$ , and stored for later use.

### **Certifications:**

South Coast Air Quality Management District: ID# 94 LA 0401

New Jersey NELAP ID: NC004

Pennsylvania DEP: Registration #68-3321

# TRIANGLE ENVIRONMENTAL SERVICES, INC.

## METHOD 3-C SAMPLE CALCULATION

Note: All pressure values have been converted when necessary to mm Hg and all temperature values to Kelvin.

Name: BT Environmental  
Project ID: Cornerstone 07-3600.00

ID#07140-25C Analyzed: 6/4/07

Sample # 1 Flare Inlet Run 1

### D A T A

Tank N419:

Volume (cu.m) = 0.004477  
Pressure Temp. (K)  
(mm Hg)  
Presampling 325.0 297.15  
Postsampling 585.0 301.15  
Final 1988.0 301.15  
Barometric 748.0  
Water Vapor 28.3

### Calibration Data:

	O2	N2	CH4	CO2
Response Factor (area units/ppmC)	28.72	31.37	25.77	36.99

### Areas:

O2	40,777	40,920	40,697
N2	220,944	221,700	221,125
CH4	1,780,501	1,780,736	1,779,515
CO2	1,742,793	1,744,494	1,744,560

### C A L C U L A T I O N S

#### Measured Concentrations (ppmC):

Cm(O2) = Area(O2) / RF(O2)  
= 40777 / 28.7 = 1419.8  
= 40920 / 28.7 = 1424.8  
= 40697 / 28.7 = 1417.0

Cm(N2) = Area(N2)/RF(N2)  
= 220944 / 31.4 = 7043.2  
= 221700 / 31.4 = 7067.3  
= 221125 / 31.4 = 7048.9

Cm(CH4) = Area(CH4)/RF(CH4)  
= 1780501 / 25.8 = 69092.0  
= 1780736 / 25.8 = 69101.1  
= 1779515 / 25.8 = 69053.7

Cm(CO2) = Area(CO2)/RF(CO2)  
= 1742793 / 37.0 = 47115.2  
= 1744494 / 37.0 = 47161.2  
= 1744560 / 37.0 = 47163.0

- 2 -

TRIANGLE ENVIRONMENTAL SERVICES, INC. ID#07140-25C

METHOD 3-C SAMPLE CALCULATION

Pressure-Temperature Ratio,  $Q(i) = P(i)/T(i)$ :

postsampling tank:  $Q(1) = 585 / 301.15 = 1.942554$   
presampling tank:  $Q(2) = 325 / 297.15 = 1.093724$   
final tank:  $Q(3) = 1988 / 301.15 = 6.601362$

Volume Sampled (dscm) =  $0.3857 \times \text{Tank Volume} \times [Q(1) - Q(2)]$   
=  $0.3857 \times .004477 \times [1.9426 - 1.0937]$   
= 0.001466

Averages and % Relative Standard Deviations (%RSD) of  $C_m$ 's are calculated.  
(%RSD of C = %RSD of  $C_m$ )

Moisture Correction Factor, MCF:

= 1 - Water Vapor Pressure/Barometric Pressure  
= 1 - 28.3/ 748.0 = 0.9622

Calculated Concentrations (ppm):

$C(O_2) = Q(3) / [Q(1) - Q(2)] \times C_m(O_2) / MCF$   
=  $6.6014 / (1.9426 - 1.0937) \times 1420.5 / 0.9622 = 11482.0$

$C(N_2) = Q(3) / [Q(1) - Q(2)] \times C_m(N_2) / MCF$   
=  $6.6014 / (1.9426 - 1.0937) \times 7053.1 / 0.9622 = 57009.1$

$C(CH_4) = Q(3) / [Q(1) - Q(2)] \times C_m(CH_4) / MCF$   
=  $6.6014 / (1.9426 - 1.0937) \times 69082.3 / 0.9622 = 558379.8$

$C(CO_2) = Q(3) / [Q(1) - Q(2)] \times C_m(CO_2) / MCF$   
=  $6.6014 / (1.9426 - 1.0937) \times 47146.5 / 0.9622 = 381076.7$

# Triangle Environmental Services, Inc.

## METHOD 3-C SAMPLE QA/QC DATA

Report #07140-25C

### DAILY ANALYZER CHECKS

#### Daily Calibration

##### Response Factor (RF) Checks

Requirement: Daily RF = Initial RF  $\pm$  20%

Triplicate injections of a mixture of O<sub>2</sub>, N<sub>2</sub>, CH<sub>4</sub>, and CO<sub>2</sub> are made before and after each batch of samples.

#### Initial Calibration/Linearity

Triplicate injections of a calibration gas is made for each compound at three levels:

	Nominal Concentrations (ppm)			Initial RF 2/5/98
O <sub>2</sub>	500	10,000	200,000	28.94
N <sub>2</sub>	500	50,000	700,000	34.69
CH <sub>4</sub>	500	50,000	500,000	28.91
CO <sub>2</sub>	500	50,000	200,000	41.14

#### Analyzer Linearity Check 2/5/98

$100 \times (1 - RF/RF_{average})$

Requirement:

max. dev. O <sub>2</sub> :	- 3.4%	$\pm$ 10%
max. dev. N <sub>2</sub> :	$\pm$ 1.5%	$\pm$ 10%
max. dev. CH <sub>4</sub> :	- 1.7%	$\pm$ 10%
max. dev. CO <sub>2</sub> :	$\pm$ 0.6%	$\pm$ 10%

### EQUIPMENT CHECKS

#### Clean Sampling Equipment Check

Tank	< 2 ppm CH <sub>4</sub>	@ 100%
	< 20 ppm CO <sub>2</sub>	@ 100%

#### Sample Tank Evacuation and Leak Check

Tank evacuated to  $\leq 10$  mm Hg absolute pressure, monitored for  $\geq 1$  hour, and passed for use if no pressure change ( $< 1$  mm Hg/hr) is noted.

#### Sample Tank Volumes

Tank weighed empty, filled with deionized distilled water (temperature recorded), and weighed to the nearest 2 g. Volume calculated based on density of water at that temperature and results recorded in permanent file.

# Triangle Environmental Services, Inc. CALIBRATION DATA FOR THE ANALYSES

Client: BT Environmental

ID#07140-25C

Project ID: Cornerstone 07-3600.00

4-JUN-7 3: Analyzer F

Precalibration Calibration

Compound	Conc.	Area(1)	Area(2)	Area(3)	Average	%RSD	RF	IRF	%Diff.
O2	24600.0	708287	704110	707485	706627	0.3%	28.72	28.94	-0.74%
N2	99500.0	3126903	3110384	3126004	3121097	0.3%	31.37	34.69	-9.58%
CH4	20500.0	529583	526818	528607	528336	0.3%	25.77	28.91	-10.85%
CO2	243000.0	9006391	8960737	9001844	8989657	0.3%	36.99	41.14	-10.08%

Postanalysis Calibration

Compound	Conc.	Area(1)	Area(2)	Area(3)	Average	RF(post)	RF(pre)	%Diff
O2	24600	704807	704479	705472	704919	28.66	28.72	-0.2%
N2	99500	3111840	3112086	3117662	3113863	31.30	31.37	-0.2%
CH4	20500	528770	527182	526224	527392	25.73	25.77	-0.2%
CO2	243000	8977658	8984236	8965516	8975803	36.94	36.99	-0.2%

Sample # 1 N419  
# 2 N272  
# 3 N229

Conc. = concentration in ppmC, %RSD = % relative standard deviation,  
RF = response factor = Average Area/Conc., IRF = response factor from initial calibration,  
%Diff. =  $\frac{RF-IRF}{IRF}$  for preanalysis/ $\frac{RF(post)-RF(pre)}{RF(pre)}$ , C2+ = propane

8.0000

7.577

15.183 16.246 17.579 19.034

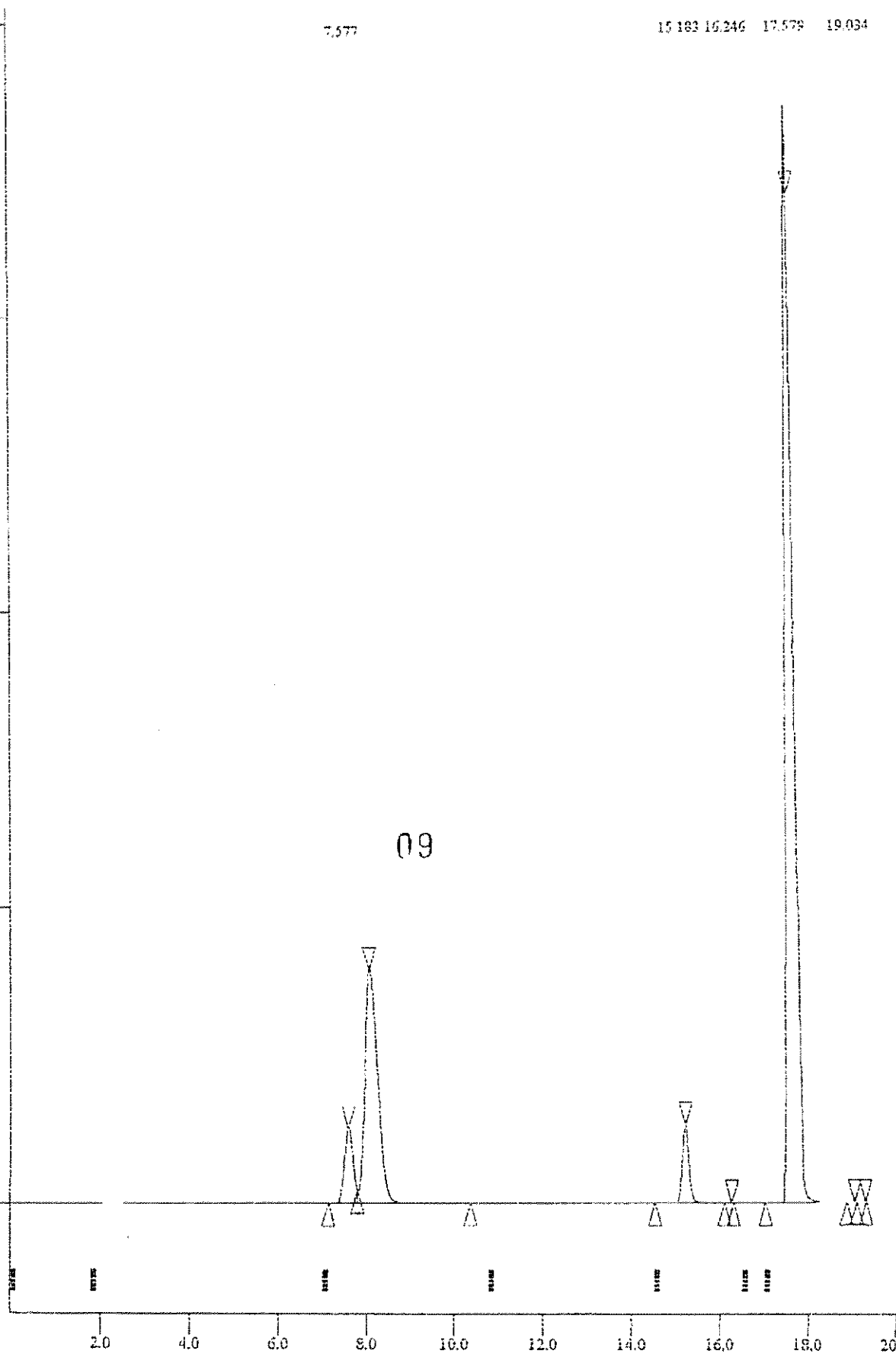
6.0000

4.0000

2.0000

0.0000

09





Title :  
 Run File : C:\STAR\RECALCF\TES\_F136.RUN  
 Method File : C:\STAR\CALTCOD.MTH  
 Sample ID : 1- 3C MIX CC93314

Injection Date: 4-JUN-7 3:19 PM      Calculation Date: 4-JUN-7 3:39 PM

Operator :                      Detector Type: ADCB (10 Volts)  
 Workstation: MS-DOS\_6          Bus Address : 16  
 Instrument : Varian Star #1      Sample Rate : 10.00 Hz  
 Channel : A = A                  Run Time : 20.002 min

\*\*\*\*\* Star Chromatography Workstation \*\*\*\*\* Version 4.5 \*\*\*\*\*

Run Mode : Analysis  
 Peak Measurement: Peak Area  
 Calculation Type: Percent

Peak No.	Peak Name	Result ( )	Ret. Time (min)	Time Offset (min)	Area (counts)	Sep. Code	Width 1/2 (sec)	Status Codes
1	O2	5.2971	7.577	-0.023	708287	EV	13.7	
2	N2	23.3854	9.055	-0.015	3126903	VB	18.5	
3	CH4	3.9606	15.183	-0.067	529583	BB	9.7	
4	CO2	67.3568	17.579	-0.021	9006391	BB	0.0	
Totals:		99.9999		-0.126	13371164			

Total Unidentified Counts :                      0 counts

Detected Peaks: 7                      Rejected Peaks: 3                      Identified Peaks: 4

Multiplier: 1                      Divisor: 1

Baseline Offset: 25 microVolts

Noise (used): 30 microVolts - fixed value  
 Noise (monitored before this run): 80 microVolts

Could not format the injection information for this run.  
 Install the driver for the module at address 17 (type 8) to format this data.

#### Revision Log:

4-JUN-7 3:39 PM: Calculated results from channel A using method:  
 'C:\STAR\CALTCOD.MTH'

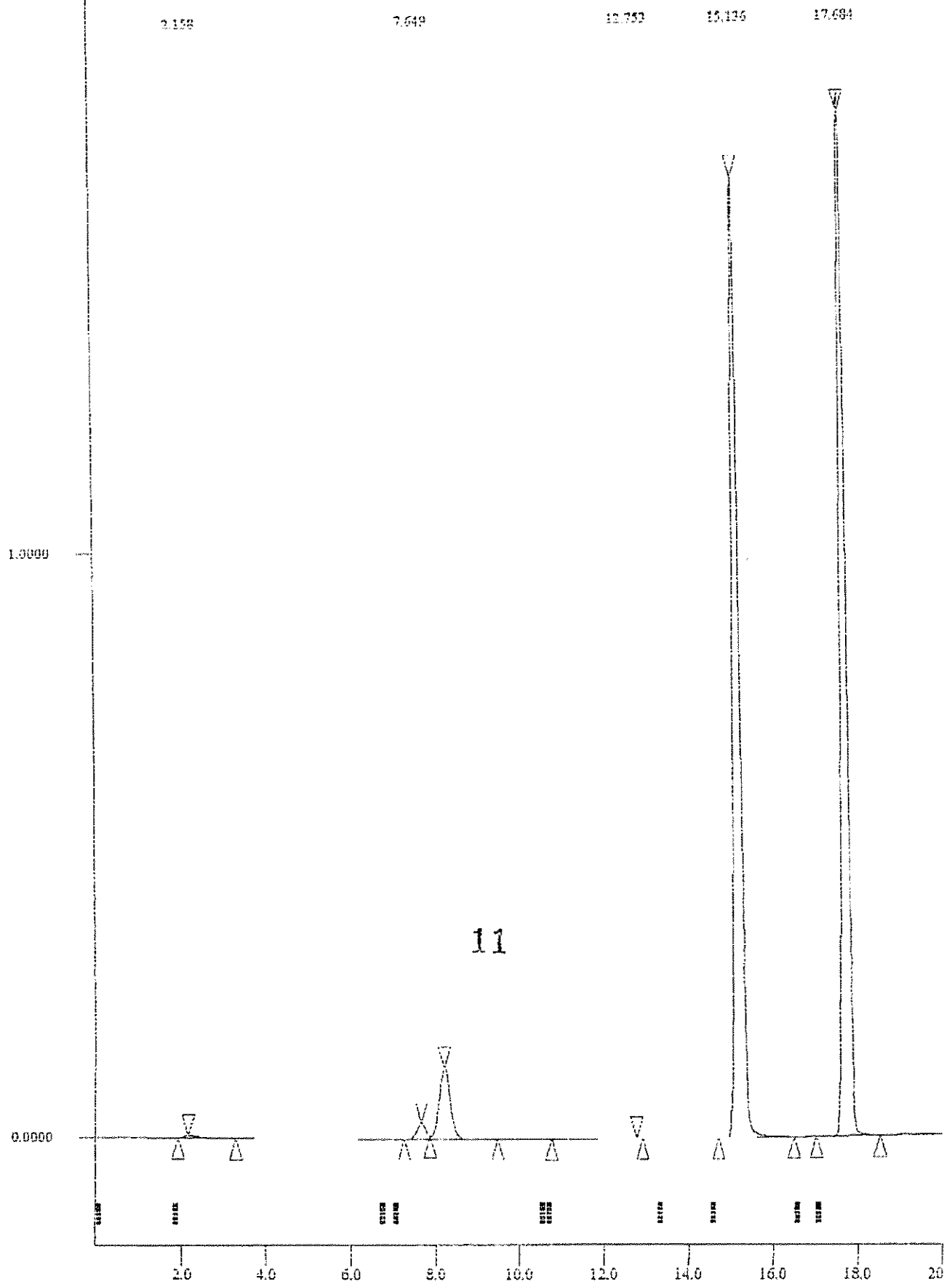
#### Error Log:

Could not format the error log for the module at address 17 (type 8).  
 Install the appropriate module driver to format this data.

ADC Board:

Original Notes:

\*\*\*\*\*



Print Date: Wed Jun 06 14:56:09 2007

Page 1 of 1

Title :  
Run File : C:\STAR\RECALCF\TES\_F139.RUN  
Method File : C:\STAR\TCD.MTH  
Sample ID : 2- tank N419

Injection Date: 4-JUN-7 4:46 PM Calculation Date: 4-JUN-7 5:06 PM

Operator : Detector Type: ADCB (10 Volts)  
Workstation: MS-DOS\_6 Bus Address : 16  
Instrument : Varian Star #1 Sample Rate : 10.00 Hz  
Channel : A - A Run Time : 20.002 min

\*\*\*\*\* Star Chromatography Workstation \*\*\*\*\* Version 4.5 \*\*\*\*\*

Run Mode : Analysis  
Peak Measurement: Peak Area  
Calculation Type: Percent

Peak No.	Peak Name	Result ( )	Ret. Time (min)	Time Offset (min)	Area (counts)	Sep. Code	Width 1/2 (sec)	Status Codes
1	O2	1.0737	7.649	0.049	40777	BV	14.8	
2	N2	5.8176	8.192	0.122	220944	VE	17.2	
3	CH4	46.8817	15.136	-0.114	1780501	BB	10.1	
4	CO2	45.8889	17.684	0.084	1742793	BB	9.3	
Totals:		99.6619		0.141	3785015			

Total Unidentified Counts : 12842 counts

Detected Peaks: 6 Rejected Peaks: 0 Identified Peaks: 4

Multiplier: 1 Divisor: 1

Baseline Offset: -9 microVolts

Noise (used): 90 microVolts - monitored before this run

Could not format the injection information for this run.  
Install the driver for the module at address 17 (type 8) to format this data.

Error Log:

Could not format the error log for the module at address 17 (type 8).  
Install the appropriate module driver to format this data.

ADC Board:

\*\*\*\*\*

# TRIANGLE ENVIRONMENTAL SERVICES, INC. METHOD 3-C DATA REPORT

Name: BT Environmental

ID#07140-25C Analyzed: 6/4/07

Project ID: Cornerstone 07-3600.00

Sample # 1 Flare Inlet Run 1

TANK N419:

Volume (cu.m) = 0.004477

	Pressure (mm Hg)	Temperature (K)	P/T
Presampling	325.0	297.15	1.094
Postsampling	585.0	301.15	1.943
Lab receipt	585.0	301.15	1.943
Final	1988.0	301.15	6.601
Barometric	748.0		
Water Vapor	28.3		

Field and laboratory postsampling pressure-temperature comparison:

Laboratory receipt P/T / Field postsampling P/T = 1.000

Volume Sampled (dscm) = 0.001466

Calibration Data:

	O2	N2	CH4	CO2
Response Factor (area units/ppmC)	28.72	31.37	25.77	36.99
Practical Quantitation Limit (ppm)	156	156	156	156

Areas:

O2	40,777	40,920	40,697
N2	220,944	221,700	221,125
CH4	1,780,501	1,780,736	1,779,515
CO2	1,742,793	1,744,494	1,744,560

Concentrations:

	ppm		%RSD
	Amount ±	SD	
O2	11482 ±	32	0.3
N2	57009 ±	102	0.2
CH4	558380 ±	203	0.0
CO2	381077 ±	219	0.1

# TRIANGLE ENVIRONMENTAL SERVICES, INC.

## METHOD 3-C DATA REPORT

Name: BT Environmental

ID#07140-25C Analyzed: 6/4/07

Project ID: Cornerstone 07-3600.00

Sample # 2 Flare Inlet Run 2

TANK N272:

Volume (cu.m) = 0.004540

	Pressure (mm Hg)	Temperature (K)	P/T
Presampling	326.0	297.15	1.097
Postsampling	600.0	301.15	1.992
Lab receipt	600.0	301.15	1.992
Final	1877.0	301.15	6.233
Barometric	748.0		
Water Vapor	28.3		

Field and laboratory postsampling pressure-temperature comparison:

Laboratory receipt P/T / Field postsampling P/T = 1.000

Volume Sampled (dscm) = 0.001568

Calibration Data:

	O2	N2	CH4	CO2
Response Factor (area units/ppmC)	28.72	31.37	25.77	36.99
Practical Quantitation Limit (ppm)	140	140	140	140

Areas:

O2	46,381	46,448	46,534
N2	251,163	250,785	251,219
CH4	1,981,391	1,978,434	1,978,260
CO2	1,941,303	1,938,610	1,941,340

Concentrations:

	ppm		%RSD
	Amount ±	SD	
O2	11704 ±	19	0.2
N2	57907 ±	54	0.1
CH4	555759 ±	494	0.1
CO2	379565 ±	306	0.1

# TRIANGLE ENVIRONMENTAL SERVICES, INC.

## METHOD 3-C DATA REPORT

Name: BT Environmental

ID#07140-25C Analyzed: 6/4/07

Project ID: Cornerstone 07-3600.00

Sample # 3 Flare Inlet Run 3

TANK N229:

Volume (cu.m) = 0.004477

	Pressure (mm Hg)	Temperature (K)	P/T
Presampling	325.0	297.15	1.094
Postsampling	592.0	301.15	1.966
Lab receipt	592.0	301.15	1.966
Final	1891.0	301.15	6.279
Barometric	748.0		
Water Vapor	28.3		

Field and laboratory postsampling pressure-temperature comparison:

Laboratory receipt P/T / Field postsampling P/T = 1.000

Volume Sampled (dscm) = 0.001506

Calibration Data:

	O2	N2	CH4	CO2
Response Factor (area units/ppmC)	28.72	31.37	25.77	36.99
Practical Quantitation Limit (ppm)	145	145	145	145

Areas:

O2	167,607	167,885	167,778
N2	717,015	718,623	718,935
CH4	1,614,451	1,617,569	1,605,055
CO2	1,590,133	1,588,794	1,576,452

Concentrations:

	ppm		%RSD
	Amount ±	SD	
O2	43712 ±	37	0.1
N2	171329 ±	246	0.1
CH4	468223 ±	1892	0.4
CO2	320690 ±	1526	0.5

# **Chain of Custody**

**Triangle Environmental Services, Inc.**  
**LABORATORY SAMPLE INFORMATION AND CHAIN-OF-CUSTODY FORM**

Company Name: <u>BTEC</u>		Project/Client ID: <u>Cornerstone # 07-36000</u>		Date: <u>5-31-07</u>
Contact Person: <u>MARK WESTERBERG</u>	Phone #: <u>734 323 9053</u>		Process Type: <u>Candlestick Flame</u>	
Latest Date Complete Set of Samples Expected at Lab:		Note: Normal Turnaround is 15 working days after receipt of complete set of samples		Results Due Date: <u>6-22-07</u>
		Report Package Due Date:		Extra charge will apply for rush results
Send Report to: <small>(Street address required for Fed Ex shipment of report)</small>	Person <u>Mark Westberg</u>		Send Invoice to: <small>(if different from report address)</small>	Person
	Company <u>BTEC</u>			Company
	Address <u>2615 W. 10th</u>			Address
	<u>Fernbach, MI 48220</u>			
Phone # <u>248 548 8070</u>		FAX # <u>248-548-8073</u>		PO#

✓ all applicable boxes

**Analysis**

US EPA: <input type="checkbox"/> Method 25 <input checked="" type="checkbox"/> Method 3-C <input type="checkbox"/> Method 25-C (NMOC as C [default]) <input type="checkbox"/> Method 10-B				SCAQMD: <input type="checkbox"/> Method 25.1 <input type="checkbox"/> Method 25.2	
# of Tank & Trap Samples:	# of Tank-Only Samples: <u>3</u>	# of Trap-Only Samples:	# of Bag Samples:		
<input type="checkbox"/> Audit with Delay <small>(extra charge)</small>	<input type="checkbox"/> Rush Turnaround <small>(extra charge)</small>	<input type="checkbox"/> High Concentrations Possible <input type="checkbox"/> Call if Concentrations High	<input type="checkbox"/> Dilute High Concentrations <small>(extra charge)</small>		
Special Instructions:					
Tanks for Analysis (Bags) (List IDs): <u>N419, N272, N229</u>			Traps for Analysis (List IDs):		
<input checked="" type="checkbox"/> TES Equipment		<input type="checkbox"/> Client Equipment		<input type="checkbox"/> Client Equipment to be Reconditioned	
Tanks, Unused for Reconditioning (List IDs): <u>N321</u>			Traps, Unused for Reconditioning (List IDs):		
Relinquished by: <u>Mark Westberg</u>		Date: <u>5-31-07</u>	Time: <u>1:30</u>	To: <small>(Carrier)</small>	
Tanks received at TES by: <u>Jeff Y. Lee</u>	Condition: <u>good</u>	Date: <u>6/1/07</u>	Time: <u>11:30</u>	Traps received at TES by:	Condition: Date: Time:



**METHOD 25 SAMPLE DATA**  
**Triangle Environmental Services, Inc.**

Company Name: <u>BT Environmental</u>		Date: <u>5/25/07</u>	
Units of Measure:	Pressure: <input checked="" type="checkbox"/> mm Hg <input type="checkbox"/> in.Hg	Temperature: <input type="checkbox"/> °F <input checked="" type="checkbox"/> °C	
Sample #	Tank ID # <u>N419</u>	Trap ID #	
Description (20 character limit)	<u>FLARE INLET RUN 1</u>		
<u>Station 10.16</u>	Barometric Pressure	Tank Vacuum	Absolute Pressure
Pre-Test Data	<u>761</u>	<u>-50 (145)</u>	<u>325</u>
Post-Test Data		<u>-14 (145)</u>	
Sample #	Tank ID # <u>N272</u>	Trap ID #	
Description (20 character limit)	<u>FLARE INLET RUN 2</u>		
<u>Station 10.18</u>	Barometric Pressure	Tank Vacuum	Absolute Pressure
Pre-Test Data	<u>761</u>	<u>-52 (15.25)</u>	<u>326</u>
Post-Test Data		<u>-13 (3.0)</u>	
Sample #	Tank ID # <u>N229</u>	Trap ID #	
Description (20 character limit)	<u>FLARE INLET RUN 3</u>		
<u>Station 10.20</u>	Barometric Pressure	Tank Vacuum	Absolute Pressure
Pre-Test Data	<u>761</u>	<u>-50 (15)</u>	<u>325</u>
Post-Test Data		<u>-15 (4)</u>	
Sample #	Tank ID # <u>N321</u>	Trap ID #	
Description (20 character limit)			
	Barometric Pressure	Tank Vacuum	Absolute Pressure
Pre-Test Data	<u>761</u>		<u>325</u>
Post-Test Data			
Sample #	Tank ID #	Trap ID #	
Description (20 character limit)			
	Barometric Pressure	Tank Vacuum	Absolute Pressure
Pre-Test Data			
Post-Test Data			
Sample #	Tank ID #	Trap ID #	
Description (20 character limit)			
	Barometric Pressure	Tank Vacuum	Absolute Pressure
Pre-Test Data			
Post-Test Data			



Client Cornerstone

Run Number Flow 1  
Time 12:00

Operators BC/MW

Date 5/31/07  
Sampling Location Flare inlet

Pitot Tube number 2 FT

Stack Dimensions - Distance A \_\_\_\_\_

Pitot Tube factor,  $C_p$  99

Stack Dimensions - Distance B \_\_\_\_\_

### Cyclonic Flow Check

Stack Diameter 14"

Bar. Pressure in Hg. \_\_\_\_\_

Stack Area, Sq ft. \_\_\_\_\_

Static Pressure in H<sub>2</sub>O +2.5

Gas Temp., °F WB 80°

% CO<sub>2</sub>

Moisture, v/v \_\_\_\_\_

Gas Temp., °F DB \_\_\_\_\_

% O2

% CO \_\_\_\_\_

% N2

	6	.14	106			
	5	.22	↓			
	4	.30				
	3	.38				
	2	.36				
	1	.32				

<b>Company</b>	Evergreen Recycling and Disposal Facility, Northwood, OH		
<b>Source Designation</b>	Flare Inlet		
<b>Test Date</b>	5/31/2007	<b>Pitot Tube Corr. Factor</b>	0.99
<b>Test Number</b>	1	<b>Moisture Content (%)</b>	3.0
<b>Operator</b>	MW/BC	<b>Condensate Volume</b>	----
<b>Barometric Pressure</b>	29.25	<b>Silica Gel Weight Gain</b>	----
<b>Stack Static Pressure</b>	2.3	<b>Gas Analysis Results:</b>	
<b>Stack Dimensions (in.)</b>	14	<b>CO<sub>2</sub></b>	38.1
<b>Traverse points</b>	6	<b>O<sub>2</sub></b>	1.1
<b>Wet-bulb temp. (°F)</b>	----	<b>N<sub>2</sub></b>	5.7
<b>Pitot Tube Number</b>	1	<b>CH<sub>4</sub></b>	55.8

Traverse Point Number	Stack Temp. (°F)	Velocity Pres. ("H <sub>2</sub> O)	Traverse Point Number	Stack Temp. (°F)	Velocity Pres. ("H <sub>2</sub> O)
6	106.0	0.14	6	106.0	0.14
5	106.0	0.22	5	106.0	0.22
4	106.0	0.32	4	106.0	0.32
3	106.0	0.38	3	106.0	0.38
2	106.0	0.36	2	106.0	0.36
1	106.0	0.32	1	106.0	0.32
106.0			106.0		

Stack Pressure (Ps "Hg)	29.42
Stack Gas Specific Gravity (Gs)	0.94
Average Stack Temperature (Ts °F)	212
Average Stack Velocity (Vs ft/minute)	2,265
Area of Stack (As ft <sup>2</sup> )	1.07
Flowrate (Actual CFM)	2,421
Flowrate (Standard CFM)	2,221
Flowrate (Dry Standard CFM)	2,154

<b>Company</b>	Evergreen Recycling and Disposal Facility, Northwood, OH		
<b>Source Designation</b>	Flare Inlet		
<b>Test Date</b>	5/31/2007	<b>Pitot Tube Corr. Factor</b>	0.99
<b>Test Number</b>	2	<b>Moisture Content (%)</b>	3.0
<b>Operator</b>	MW/BC	<b>Condensate Volume</b>	----
<b>Barometric Pressure</b>	29.25	<b>Silica Gel Weight Gain</b>	----
<b>Stack Static Pressure</b>	2.3	<b>Gas Analysis Results:</b>	
<b>Stack Dimensions (in.)</b>	14	<b>CO<sub>2</sub></b>	38.0
<b>Traverse points</b>	6	<b>O<sub>2</sub></b>	1.2
<b>Wet-bulb temp. (°F)</b>	----	<b>N<sub>2</sub></b>	5.8
<b>Pitot Tube Number</b>	1	<b>CH<sub>4</sub></b>	55.6

Traverse Point Number	Stack Temp. (°F)	Velocity Pres. ("H <sub>2</sub> O)	Traverse Point Number	Stack Temp. (°F)	Velocity Pres. ("H <sub>2</sub> O)
6	106.0	0.14	6	106.0	0.14
5	106.0	0.22	5	106.0	0.22
4	106.0	0.32	4	106.0	0.32
3	106.0	0.38	3	106.0	0.38
2	106.0	0.36	2	106.0	0.36
1	106.0	0.32	1	106.0	0.32
106.0			106.0		

Stack Pressure (Ps "Hg)	29.42
Stack Gas Specific Gravity (Gs)	0.94
Average Stack Temperature (Ts °F)	212
Average Stack Velocity (Vs ft/minute)	2,266
Area of Stack (As ft <sup>2</sup> )	1.07
Flowrate (Actual CFM)	2,422
Flowrate (Standard CFM)	2,222
Flowrate (Dry Standard CFM)	2,155

<b>Company</b>	Evergreen Recycling and Disposal Facility, Northwood, OH		
<b>Source Designation</b>	Flare Inlet		
<b>Test Date</b>	5/31/2007	<b>Pitot Tube Corr. Factor</b>	0.99
<b>Test Number</b>	3	<b>Moisture Content (%)</b>	3.0
<b>Operator</b>	MW/BC	<b>Condensate Volume</b>	----
<b>Barometric Pressure</b>	29.25	<b>Silica Gel Weight Gain</b>	----
<b>Stack Static Pressure</b>	2.3	<b>Gas Analysis Results:</b>	
<b>Stack Dimensions (in.)</b>	14	<b>CO<sub>2</sub></b>	32.1
<b>Traverse points</b>	6	<b>O<sub>2</sub></b>	4.4
<b>Wet-bulb temp. (°F)</b>	----	<b>N<sub>2</sub></b>	17.1
<b>Pitot Tube Number</b>	1	<b>CH<sub>4</sub></b>	46.8

Traverse Point Number	Stack Temp. (°F)	Velocity Pres. ("H <sub>2</sub> O)	Traverse Point Number	Stack Temp. (°F)	Velocity Pres. ("H <sub>2</sub> O)
6	106.0	0.14	6	106.0	0.14
5	106.0	0.22	5	106.0	0.22
4	106.0	0.32	4	106.0	0.32
3	106.0	0.38	3	106.0	0.38
2	106.0	0.36	2	106.0	0.36
1	106.0	0.32	1	106.0	0.32
106.0			106.0		

Stack Pressure (Ps "Hg)	29.42
Stack Gas Specific Gravity (Gs)	0.95
Average Stack Temperature (Ts °F)	212
Average Stack Velocity (Vs ft/minute)	2,258
Area of Stack (As ft <sup>2</sup> )	1.07
Flowrate (Actual CFM)	2,414
Flowrate (Standard CFM)	2,214
Flowrate (Dry Standard CFM)	2,148

1.000000

2.000000

3.000000

4.000000

5.000000

6.000000

7.000000

8.000000

9.000000

10.000000

11.000000

12.000000

13.000000

14.000000

15.000000

16.000000

17.000000

18.000000

19.000000

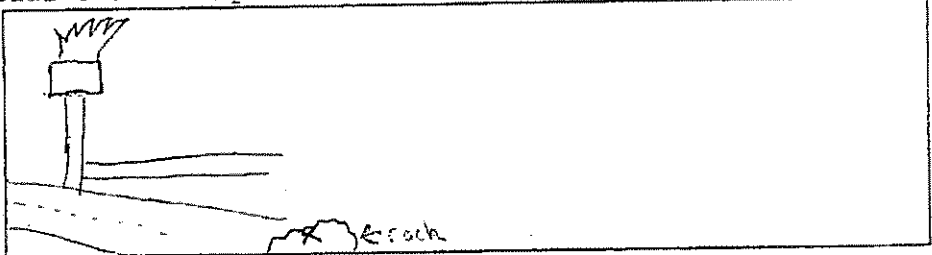
FUGITIVE OR SMOKE EMISSION INSPECTION OUTDOOR LOCATION			
Company <u>Cornerstone</u> Location <u>Evergreen Recycling and Disposal Facility</u> Company Rep. _____		Observer <u>BC</u> Affiliation <u>BIEC</u> Date <u>5-31-07</u>	
Sky Conditions <u>Clear and Sunny</u> Precipitation <u>None</u>		Wind Direction <u>NA</u> Wind Speed <u>0</u>	
Industry _____		Process Unit _____	
Sketch process unit: indicate observer position relative to source; indicate potential emission points and/or actual emission points.			
			
OBSERVATIONS	Clock Time	Observation period duration, min:sec	Accumulated emission time, min:sec
Begin Observation	<u>10:00</u>	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
End Observation	<u>12:00</u>	_____	_____

Figure 22-1





## SAMPLE CALCULATIONS

### Stack Gas Velocity

Absolute Stack Gas Temperature,  $T_s$  ( $^{\circ}$ R)

$$T_s = 460 + t_s$$

Where:  $t_s$  = Measured stack gas temperature ( $^{\circ}$ F)

For example, for the first flow measurement performed on the flare stack, the average stack temperature was  $106^{\circ}$ F. The average temperature in degrees Rankine is therefore  $106 + 460 = 566^{\circ}$ R.

Absolute Stack Gas Pressure,  $P_s$  (in. Hg)

$$P_s = P_{bar} + \left( \frac{P_{stat}}{13.6} \right)$$

Where:  $P_{bar}$  = Barometric pressure at test site (in. Hg)  
 $P_{stat}$  = Stack static pressure (in. Hg)

For example, for the first flow measurement performed on the flare stack, the barometric and stack static pressures were 30.11" Hg, and 2.5"H<sub>2</sub>O, respectively. The absolute stack pressure is then:

$$P_s = 30.11 + \left( \frac{2.5}{13.6} \right) = 30.29" \text{ Hg}$$

Stack Gas Molecular Weight, Dry Basis (lb/lb mole)

$$M_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) + 0.16(\%CH_4)$$

For example, the O<sub>2</sub> content of the flare inlet gas stream was 1.1%. The CO<sub>2</sub> content of the gas stream was 38.1%, and the N<sub>2</sub> content was 5.7%. The methane content was 55.8%<sup>1</sup>. The dry stack gas molecular weight is therefore:

$$M_d = 0.44(38.1\%) + 0.32(1.1\%) + 0.28(5.7\%) + 0.16(55.8\%) = 27.64 \frac{\text{lb}}{\text{lb mol}}$$

---

Stack Gas Molecular Weight, Wet Basis (lb/lb mole)

$$M_s = M_d \left( 1 - \frac{B_{ws}}{100} \right) + 18 \left( \frac{B_{ws}}{100} \right)$$

The stack gas moisture content from the USEPA Method 3C analysis was 3.8%. The wet stack gas molecular weight is then:

$$M_s = 27.64 \frac{\text{lb}}{\text{lb mol}} (1 - 0.038) + 18(0.038) = 27.27 \frac{\text{lb}}{\text{lb mol}}$$

Stack Gas Exit Velocity,  $V_s$  (fps)

$$V_s = K_p C_p \sqrt{\frac{\Delta P T_s}{P_s M_s}}$$

Where:  $K_p$  = Pitot tube constant equal to  $85.49 \frac{\text{ft}}{\text{sec}} \sqrt{\frac{(\text{lb/lb mole})(\text{in.Hg})}{(^{\circ}\text{R})(\text{in.H}_2\text{O})}}$   
 $C_p$  = Pitot tube coefficient, dimensionless  
 $\Delta P$  = Velocity head of stack gas (in.  $\text{H}_2\text{O}$ )  
 $M_s$  = Molecular weight of the stack gas, wet basis (lb/lb mole)

For example, for the first flow measurement performed on the flare stack the average velocity head of the stack gas was 0.29"  $\text{H}_2\text{O}$ . The diameter of the inlet duct where flow measurements were made is 14". Using values already calculated, the average stack gas velocity at the point of measurement was calculated as follows:

$$V_s = \left( 85.49 \frac{\text{ft}}{\text{sec}} \sqrt{\frac{(\text{lb/lb mol})(\text{in.Hg})}{(^{\circ}\text{R})(\text{in.H}_2\text{O})}} \right) (0.99) \sqrt{\frac{(0.29 \text{ in.H}_2\text{O})(566^{\circ}\text{R})}{(30.29 \text{ in.Hg}) \left( 27.64 \frac{\text{lb}}{\text{lb mol}} \right)}} = 37.3 \frac{\text{ft}}{\text{sec}}$$

The cross-sectional area of the inlet duct at the point of measurement is:

$$\frac{\pi}{4} \left( \frac{14 \text{ in}}{12 \frac{\text{in}}{\text{ft}}} \right)^2 = 1.07 \text{ ft}^2$$

The stack gas volumetric flowrate is then:

$$(1.07 \text{ ft}^2) \left( 37.3 \frac{\text{ft}}{\text{sec}} \right) = 39.9 \frac{\text{ft}^3}{\text{sec}}$$

The flare tip inner diameter is 14". The cross-sectional area of the flare tip is then:

$$\frac{\pi}{4} \left( \frac{14 \text{ in}}{12 \frac{\text{in}}{\text{ft}}} \right)^2 = 1.07 \text{ ft}^2$$

The flare gas exit velocity is then:

$$\frac{39.9 \frac{\text{ft}^3}{\text{sec}}}{1.07 \text{ ft}^2} = 37.3 \frac{\text{ft}}{\text{sec}}$$

### Stack Gas Net Heating Value

$$H_T = K \sum_{i=1}^n C_i H_i$$

Where:  $H_T$  = net heating value of the sample (MJ/scm)

$$K = 1.740 \cdot 10^{-7} \left( \frac{1}{\text{ppm}} \right) \left( \frac{\text{g mole}}{\text{scm}} \right) \left( \frac{\text{MJ}}{\text{kcal}} \right)$$

$C_i$  = concentration of component i on a wet basis (ppm)

$H_i$  = net heat of combustion of sample component i (kcal/g mole at 25°C and 760 mm Hg)

For example, the first USEPA Method 3C sample taken was 558,380 ppm methane. The heating value for methane in the USEPA Office of Air Quality Planning and Standards' Control Cost Manual is 11.9533 kcal/g. The molecular weight of methane is 16 g/g mole. The net heat of combustion of methane is then:

$$11.9533 \frac{\text{kcal}}{\text{g}} \left( 16 \frac{\text{g}}{\text{g mole}} \right) = 191.25 \frac{\text{kcal}}{\text{g mole}}$$

The net heating value of the sample gas stream is then:

$$H_T = 1.740 \cdot 10^{-7} \left[ \left( \frac{1}{\text{ppm}} \right) \left( \frac{\text{g mole}}{\text{scm}} \right) \left( \frac{\text{MJ}}{\text{kcal}} \right) \right] (558,380 \text{ ppm}) \left( 191.25 \frac{\text{kcal}}{\text{g mole}} \right) = 18.58 \frac{\text{MJ}}{\text{scm}}$$